## Selection for linear structure models with different variances

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#### abstract

This paper is concerned with selection of some linear structure models with different variances. The models are based on the study of relationships between two fracture toughness testing methods of dental luting cemments. The measurements are made by using several kinds of materials. They are assumed to have different variances depending on the materials, but they have the same variance between two testing methods. For such data, we consider three types of structures between two methods: (1) proportionality, (2) linearity, and (3) no structure. We give Akaike information criterion, AIC, to evaluate these models. Then, we derive corrected AIC (CAIC) which is useful for small samples. By simulation experiments, we find that CAIC is more effective than AIC in the case of small samples. Our results are applied to a real data of dental luting cements.

## 1 Introduction

This paper is concerned with selection of linear structure models with different variances. The models are based on the study of relationships between two fracture toughness testing methods of dental luting comments, by using several kinds of materials. Such an example is given in Section 5. Suppose that two testing methods are examined by using m materials. Let

$$X_{ijk}, i = 1, 2; j = 1, \dots, m; k = 1, \dots, n_{ij},$$
 (1.1)

be the kth measurement of the *j*th material by the *i*th testing method. It is assumed that  $X_{ij1}, \ldots, X_{ijn_{ij}}$  are independently and identically distributed as  $N(\mu_{ij}, \sigma_j^2)$ , i.e., for i = 1, 2 and  $j = 1, \ldots, m$ ,

$$X_{ijk} \sim N(\mu_{ij}, \sigma_j^2), \ k = 1, \dots, n_{ij}.$$
 (1.2)

The data are expressed as in Table 1 below.

method $i$	material $j$		sample	mean	variance	
	1	$x_{111}$	• • •	$x_{11n_{11}}$	$\mu_{11}$	$\sigma_1^2$
1	•	÷		•	÷	÷
	m	$x_{1m1}$	•••	$x_{1mn_{1j}}$	$\mu_{1m}$	$\sigma_m^2$
	1	$x_{211}$	• • •	$x_{21n_{21}}$	$\mu_{21}$	$\sigma_1^2$
2	:	÷		:	:	÷
	m	$x_{2m1}$	•••	$x_{2mn_{2j}}$	$\mu_{2m}$	$\sigma_m^2$

Table 1. The data on toughness testing methods by using diffent dental luting cements

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Now we are intersting wheter there is a linear structure between  $(\mu_{11}, \ldots, \mu_{1m})$  and  $(\mu_{21}, \ldots, \mu_{2m})$ or not. For that purpose we consider three types of structure models:

$$M_{1}: \ \mu_{2j} = \gamma \mu_{1j}, \ \gamma \neq 0, \quad j = 1, \cdots, m,$$
  

$$M_{2}: \ \mu_{2j} = \beta \mu_{1j} + \alpha, \ \beta \neq 0, \quad j = 1, \cdots, m,$$
  

$$M_{3}: \text{ otherwise,}$$

$$(1.3)$$

where  $\gamma$ ,  $\alpha$  and  $\beta$  are unknown. The models  $M_1$  and  $M_2$  show that two methods are essentially the same, though their relationships are different. We apply Akaike information criterion (AIC, Akaike (1973)) to evaluate these models. Various linear functional relationships have been considered, see e.g. Anderson (1984), Fuller (1987). However, it may be noted that the linear functional relationship as in  $M_1$  and  $M_2$  has not been discussed.

The AIC is given in Section 2. In Section 3 we study the risk and the bias of AIC, and propose a corrected AIC, i.e., CAIC. In Section 4, two criteria AIC and CAIC are compared by simulation experiments. It is shown that CAIC is more effective than AIC in the case of small samples. In Section 5, we give an example of two fracture toughness testing methods by using six dental luting cemments.

#### 2 Derivation of AIC

In general, AIC was proposed as a criterion of evaluating a model by Akaike (1973). Let  $\boldsymbol{x}$  and  $\boldsymbol{\theta}$  be the column vectors of all the observations  $x_{ijk}$  and the parameters  $\mu_{ij}$  and  $\sigma_j^2$ , respectively. Let the log-likelihood be denoted by  $\ell(\boldsymbol{\theta}|\boldsymbol{x})$ . Then, AIC is given by

$$AIC = -2\ell(\hat{\boldsymbol{\theta}}|\boldsymbol{x}) + 2d, \tag{2.1}$$

where  $\hat{\theta}$  is the maximum likelihood estimator (MLE) of  $\theta$ , and d is the dimension of a model, or the number of independent parameters involved in a model.

Let  $d_1$ ,  $d_2$  and  $d_3$  be the dimension d for models  $M_1$ ,  $M_2$  and  $M_3$  given in (1.3), respectively. Then, the dimensions are as follows:

$$d_1 = 2m + 1$$
,  $d_2 = 2m + 2$ ,  $d_3 = 3m$ . (2.2)

The density function of  $X_{ijk}$  is

$$f(x_{ijk}|\mu_{ij},\sigma_j^2) = \frac{1}{\sqrt{2\pi\sigma_j^2}} \exp\left\{-\frac{1}{2} \frac{(x_{ijk}-\mu_{ij})^2}{\sigma_j^2}\right\},\,$$

since  $X_{ijk}$  is distributed as  $N(\mu_{ij}, \sigma_i^2)$ . Then, the log-likelihood function of  $\boldsymbol{\theta}$  is

$$\ell(\boldsymbol{\theta}|\boldsymbol{x}) = \log \prod_{i=1}^{2} \prod_{j=1}^{m} \prod_{k=1}^{n} f(x_{ijk}|\mu_{ij}, \sigma_{j}^{2})$$
  
$$= -\frac{1}{2} \sum_{j=1}^{m} \{n_{j} \log 2\pi + n_{j} \log \sigma_{j}^{2}\}$$
  
$$-\frac{1}{2} \sum_{i=1}^{2} \sum_{j=1}^{m} \frac{1}{\sigma_{j}^{2}} \sum_{k=1}^{n_{ij}} (x_{ijk} - \mu_{ij})^{2},$$
  
(2.3)

where  $n_j = n_{1j} + n_{2j}$ , j = 1, ..., m. Let  $\hat{\sigma}_{j;a}^2$  be the MLE of  $\sigma_j^2$  under the model  $M_a$ . Then, the AIC for  $M_a$  is expressed as

$$AIC_a = \sum_{j=1}^m n_j \log \hat{\sigma}_{j;a}^2 + n\{\log(2\pi) + 1\} + 2d_a, \ a = 1, 2, 3,$$
(2.4)

where  $n = n_1 + \cdots + n_m$ . In the following, we give the MLE's of the unknown parameters as well as  $\sigma_i^2$  under  $M_1, M_2$  and  $M_3$ . Let

$$\bar{x}_{ij} = \frac{1}{n_{ij}} \sum_{k=1}^{n_{ij}} x_{ijk}, \ s_{ij}^2 = \frac{1}{n_{ij}} \sum_{k=1}^{n_{ij}} (x_{ijk} - \bar{x}_{ij})^2.$$

For simplicity, first consider the case  $M_3$ . The independent unknown parameters are  $\mu_{1j}, \mu_{2j}$  and  $\sigma_j^2$ , and it is easy to see that their MLE's are given by

$$\hat{\mu}_{1j} = \bar{x}_{1j}, \ \hat{\mu}_{2j} = \bar{x}_{2j}, \ \hat{\sigma}_j^2 = \frac{1}{n_j} (n_{1j} s_{1j}^2 + n_{2j} s_{2j}^2).$$
 (2.5)

Therefore, the  $\hat{\sigma}_{j;3}^2$  in (2.4) is given by

$$\hat{\sigma}_{j;3}^2 = \frac{1}{n_j} (n_{1j} s_{1j}^2 + n_{2j} s_{2j}^2), \ j = 1, \dots, m.$$
(2.6)

Next consider the case  $M_1$ . The independent unknown parameters are  $\mu_{1j}$ ,  $\gamma$  and  $\sigma_j^2$ . It is shown that the MLE's are solutions of the following likelihood equations:

$$\frac{\partial}{\partial \mu_{ij}} \ell(\boldsymbol{\theta} | \boldsymbol{x}) = 0, \ \frac{\partial}{\partial \sigma_j^2} \ell(\boldsymbol{\theta} | \boldsymbol{x}) = 0, \ \frac{\partial}{\partial \gamma} \ell(\boldsymbol{\theta} | \boldsymbol{x}) = 0.$$

Solving the likelihood equations  $(\partial/\partial \mu_{1j})\ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0$ ,

$$-\frac{1}{2}\frac{1}{\sigma_j^2} \left\{ -2\sum_{k=1}^{n_{1j}} (x_{1jk} - \mu_{1j}) - 2\gamma \sum_{k=1}^{n_{2j}} (x_{2jk} - \gamma \mu_{1j}) \right\} = 0,$$
  

$$\Leftrightarrow (n_{1j}\bar{x}_{1j} + \gamma n_{2j}\bar{x}_{2j}) - (n_{1j} + \gamma^2 n_{2j})\mu_{1j} = 0,$$
  

$$\Leftrightarrow \mu_{1j} = \frac{1}{n_{1j} + \gamma^2 n_{2j}} (n_{1j}\bar{x}_{1j} + \gamma n_{2j}\bar{x}_{2j}).$$
(2.7)

Similarly, solving  $(\partial/\partial \sigma_j^2)\ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0$ ,

$$-\frac{n_j}{2}\frac{1}{\sigma_j^2} + \frac{1}{2}\frac{1}{(\sigma_j^2)^2} \left\{ \sum_{k=1}^{n_{1j}} (x_{1jk} - \mu_{1j})^2 + \sum_{k=1}^{n_{2j}} (x_{2jk} - \gamma\mu_{1j})^2 \right\} = 0,$$
  
$$\Leftrightarrow \sigma_j^2 = \frac{1}{n_j} \left\{ \sum_{k=1}^{n_{1j}} (x_{1jk} - \mu_{1j})^2 + \sum_{k=1}^{n_{2j}} (x_{2jk} - \gamma\mu_{1j})^2 \right\}.$$
 (2.8)

Sustituting (2.7) for (2.8), we have

$$\sigma_j^2 = \frac{1}{n_j (n_{1j} + \gamma^2 n_{2j})} \left\{ (n_{1j} + \gamma^2 n_{2j}) (n_{1j} s_{1j}^2 + n_{2j} s_{2j}^2) + n_{1j} n_{2j} (\gamma \bar{x}_{1j} - \bar{x}_{2j})^2 \right\}.$$
(2.9)

Substituting (2.7) and (2.9) for the likelihood equation  $(\partial/\partial\gamma)\ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0$ , and simplifying the resultant equation, we find that the MLE  $\hat{\gamma}$  of  $\gamma$  is a solution of

$$\sum_{j=1}^{m} \frac{(n_{1j}\bar{x}_{1j} + \gamma n_{2j}\bar{x}_{2j})(\gamma\bar{x}_{1j} - \bar{x}_{2j})}{(n_{1j} + \gamma^2 n_{2j})(n_{1j}s_{1j}^2 + n_{2j}s_{2j}^2) + n_{1j}n_{2j}(\gamma\bar{x}_{1j} - \bar{x}_{2j})^2} \times \frac{n_j n_{1j}n_{2j}}{n_{1j} + \gamma^2 n_{2j}} = 0.$$
(2.10)

Note that  $\hat{\mu}_{1j}$  and  $\hat{\sigma}_j^2 = \hat{\sigma}_{j;1}^2$  are given by (2.7) and (2.9) with  $\gamma = \hat{\gamma}$ , respectively.

Finally consider the case  $M_2$ . The independent unknown parameters are  $\mu_{1j}, \alpha, \beta$  and  $\sigma_j^2$ . The MLE's are solutions of the following likelihood equations:

$$\frac{\partial}{\partial \mu_{1j}} \ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0, \ \frac{\partial}{\partial \sigma_j^2} \ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0, \ \frac{\partial}{\partial \alpha} \ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0, \ \frac{\partial}{\partial \beta} \ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0.$$

Solving the likelihood equations  $(\partial/\partial \mu_{1j})\ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0$ ,

$$-\frac{1}{2}\frac{1}{\sigma_j^2} \left\{ -2\sum_{k=1}^{n_{1j}} (x_{1jk} - \mu_{1j}) - 2\beta \sum_{k=1}^{n_{2j}} (x_{2jk} - \alpha - \beta \mu_{1j}) \right\} = 0,$$
  

$$\Leftrightarrow (n_{1j}\bar{x}_{1j} + \beta n_{2j}\bar{x}_{2j} - \alpha \beta n_{2j}) - (n_{1j} + \beta^2 n_{2j})\mu_{1j} = 0,$$
  

$$\Leftrightarrow \mu_{1j} = \frac{1}{n_{1j} + \beta^2 n_{2j}} (n_{1j}\bar{x}_{1j} + \beta n_{2j}\bar{x}_{2j} - \alpha \beta n_{2j}).$$
(2.11)

Similarly, solving  $(\partial/\partial \sigma_j^2)\ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0$ ,

$$-\frac{n_j}{2}\frac{1}{\sigma_j^2} + \frac{1}{2}\frac{1}{(\sigma_j^2)^2} \left\{ \sum_{k=1}^{n_{1j}} (x_{1jk} - \mu_{1j})^2 + \sum_{k=1}^{n_{2j}} (x_{2jk} - \alpha - \beta\mu_{1j})^2 \right\} = 0,$$
  
$$\Leftrightarrow \sigma_j^2 = \frac{1}{n_j} \left\{ \sum_{k=1}^{n_{1j}} (x_{1jk} - \mu_{1j})^2 + \sum_{k=1}^{n_{2j}} (x_{2jk} - \alpha - \beta\mu_{1j})^2 \right\}.$$
 (2.12)

Sustituting (2.11) for (2.12), we have

$$\sigma_j^2 = \frac{1}{n_j(n_{1j} + \beta^2 n_{2j})} \left\{ (n_{1j} + \beta^2 n_{2j})(n_{1j} s_{1j}^2 + n_{2j} s_{2j}^2) + n_{1j} n_{2j} (\bar{x}_2 - \alpha - \beta \bar{x}_{1j})^2 \right\}.$$
(2.13)

Substituting (2.11) and (2.13) for the likelihood equations  $(\partial/\partial \alpha)\ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0$  and  $(\partial/\partial \beta)\ell(\boldsymbol{\theta}|\boldsymbol{x}) = 0$ , and simplifying the resultant equations, we find that the MLE's  $\hat{\alpha}$  and  $\hat{\beta}$  of  $\alpha$  and  $\beta$  are solutions of

$$\sum_{j=1}^{m} \frac{n_j n_{1j} n_{2j} (\bar{x}_{2j} - \alpha - \beta \bar{x}_{1j})}{(n_{1j} + \beta^2 n_{2j})(n_{1j} s_{1j}^2 + n_{2j} s_{2j}^2) + n_{1j} n_{2j} (\bar{x}_{2j} - \alpha - \beta \bar{x}_{1j})^3} = 0.$$
(2.14)  
$$\sum_{j=1}^{m} \frac{(n_{1j} \bar{x}_{1j} + \beta n_{2j} \bar{x}_{2j} - \alpha \beta n_{2j})(\bar{x}_{2j} - \alpha - \beta \bar{x}_{1j})}{(n_{1j} + \beta^2 n_{2j})(n_{1j} s_{1j}^2 + n_{2j} s_{2j}^2) + n_{1j} n_{2j} (\bar{x}_{2j} - \alpha - \beta \bar{x}_{1j})^2} \times \frac{n_j n_{1j} n_{2j}}{n_{1j} + \beta^2 n_{2j}} = 0.$$
(2.15)

Note that  $\hat{\mu}_{1j}$  and  $\hat{\sigma}_j^2 = \hat{\sigma}_{j;2}^2$  are given by (2.11) and (2.13) with  $\alpha = \hat{\alpha}$  and  $\beta = \hat{\beta}$ , respectively.

## 3 The bias of AIC and its correction

In general, AIC was introduced as an asymptotically unbiased estimator of the predictive risk function of a model. Let X be a random vector whose components consists of all the random variables  $X_{ijk}$ . In our model the risk function is expressed as

$$R_A = E_{\boldsymbol{Y}}^* E_{\boldsymbol{X}}^* [-2\ell(\hat{\boldsymbol{\theta}}|\boldsymbol{Y})]$$
(3.1)

where  $\boldsymbol{Y}$  is a random vector whose componets consist of all the future variables  $Y_{ijk}$  corresponding to  $X_{ijk}$ . It is assumed that  $\boldsymbol{Y}$  has the same distribution as  $\boldsymbol{X}$  and is independent of  $\boldsymbol{X}$ . The expectation  $E^*$  denotes the one with respect to the true model. The bias when we estimate the risk function by  $-2\ell(\hat{\boldsymbol{\theta}}|X)$  is written as

$$B_A = E_{\boldsymbol{Y}}^* E_{\boldsymbol{X}}^* [-2\ell(\hat{\boldsymbol{\theta}}|\boldsymbol{Y}) + 2\ell(\hat{\boldsymbol{\theta}}|\boldsymbol{X})].$$
(3.2)

AIC uses 2d as an estimator of  $B_A$ . Sugiura (1978) obtained more precise expressions of  $B_A$  for some models, assuming that the true model is included in the model considered. The AIC with such biases is called CAIC. Further, Fujikoshi and Satoh (1997) proposed to estimate  $B_A$ , relaxing the assumption that the true model is included in the candidate model. The bias of AIC in our model is

$$B_{A} = \sum_{j=1}^{m} (n_{j}\sigma_{j}^{2})E\left[\frac{1}{\hat{\sigma}_{j}^{2}}\right] - n + E\left[\frac{1}{\hat{\sigma}_{j}^{2}}\left\{n_{1j}(\mu_{1j} - \hat{\mu}_{1j})^{2} + n_{2j}(\mu_{2j} - \hat{\mu}_{2j})^{2}\right\}\right],$$
(3.3)

where the  $\hat{\mu}_{2j}$  in the cases  $M_1$  and  $M_2$  are  $\hat{\gamma}\hat{\mu}_{1j}$  and  $\hat{\alpha} + \hat{\beta}\hat{\mu}_{1j}$ , respectively.

Let  $B_{A;a}$  be the bias  $B_A$  for model  $M_a$ . Assume that  $n_{ij} = n_0$  for all i = 1, 2 and  $j = 1, \ldots, m$ . Then, it is shown that  $B_{A;a}$  can be expanded as follows:

$$B_{A;1} = d_1 + \frac{1}{n_0}c_1 + O(n_0^{-2}),$$
  

$$B_{A;2} = d_2 + \frac{1}{n_0}c_2 + O(n_0^{-2}),$$
  

$$B_{A;2} = d_3 + \frac{1}{n_0}c_3 + O(n_0^{-2}),$$
  
(3.4)

where

$$c_{1} = 4(m+2) + \frac{4(m-1)}{1+\gamma^{2}} \frac{1}{t_{2,2}} - 2\frac{t_{4,4}}{t_{2,2}^{2}},$$

$$c_{2} = 4(m+4) + \frac{4(m-2)}{1+\beta^{2}} \frac{t_{0,2}}{t_{0,2}t_{2,2} - t_{1,2}^{2}} - \frac{2R}{\left(t_{0,2}t_{2,2} - t_{1,2}^{2}\right)^{2}},$$

$$c_{3} = 10m.$$

and  $t_{p,q} = \sum_{j=1}^{m} \mu_{1j}^p / \sigma_j^q$ ,

$$R = t_{4,4}t_{0,2}^2 + 2t_{2,2}t_{2,4}t_{0,2} - 4t_{1,2}t_{3,4}t_{0,2} + t_{0,4}t_{2,2}^2 - 4t_{1,2}t_{1,4}t_{2,2} + 4t_{1,2}^2t_{2,4}.$$

Using the above results, a corrected AIC is defined as

$$CAIC_a = AIC_a + \frac{1}{n_0}\hat{c}_a, \ a = 1, 2, 3,$$
(3.5)

where  $\hat{c}_a$  is defined from  $c_a$  by substituting MLE's for the unknown parameters.

## 4 Simulation study

In order to investigate the actual behavior of AIC and CAIC, we examined their average biases and frequencies selected by simulation experiments. The simulations were made for the cases where the sample sizes  $n_{ij}$  are the same as  $n_0$ , and  $n_0 = 6, 10, 30, 50, 100$ . The parameters are defined as follows:

$$\begin{split} \gamma &= 1.05, \quad \beta = 1.05, \quad \alpha = 0.05 \\ \mu_{11} &= 0.07, \quad \mu_{12} = 0.10, \quad \mu_{13} = 0.20, \\ \mu_{14} &= 0.70, \quad \mu_{15} = 1.00, \quad \mu_{16} = 2.00, \\ \sigma_1^2 &= 0.00007, \quad \sigma_2^2 = 0.00100, \quad \sigma_3^2 = 0.00400, \\ \sigma_4^2 &= 0.00600, \quad \sigma_5^2 = 0.01000, \quad \sigma_6^2 = 0.03000. \end{split}$$

The numbers of iterations were set as 10,000. Tables 2 and 3 are frequencies of model selected by AIC and CAIC in the case that  $M_1$  is true. Tables 4 and 5 show the ones in the case that  $M_2$  is true. Figures 1 and 2 show the differences between the average of the true risk and the average of each of AIC and CAIC. Figure 1 shows the case that  $M_1$  is true, and Figure 2 shows the case that  $M_2$  is true. From these experiments, we can see that CAIC is more effective than AIC in the case of small samples.

Table 2. AIC when $M_1$ is true					Table 3. CAIC when $M_1$ is true				
	M1	M2	M3	-	M1(CAIC)	M1	M2	M3	
$n_0 = 6$	7559	1271	1170	-	$n_0 = 6$	9017	732	251	
$n_0 = 10$	7883	1244	873		$n_0 = 10$	8838	847	315	
$n_0 = 30$	7820	1480	700		$n_0 = 30$	8222	1319	459	
$n_0 = 50$	7935	1392	673		$n_0 = 50$	8169	1301	530	
$n_0 = 100$	8018	1359	623	_	$n_0 = 100$	8123	1312	565	

Table 4. AIC when $M_2$ is true					Table 5. CAIC when $M_2$ is true				
	M1	M2	M3	-		M1	M2	M3	
$n_0 = 6$	0	8166	1834	-	$n_0 = 6$	0	9425	575	
$n_0 = 10$	0	8615	1385		$n_0 = 10$	0	9374	626	
$n_0 = 30$	0	8955	1045		$n_0 = 30$	0	9195	805	
$n_0 = 50$	0	9020	980		$n_0 = 50$	0	9187	813	
$n_0 = 100$	0	9034	966	_	$n_0 = 100$	0	9121	879	





Figure 1. Diferences between risks when  $M_1$  is true





#### 5 An example

We consider the data (Kanai et al. (2007)) measured for different 6 materials by two fracture toughness testing methods. The sample sizes are all 6. The sample means and variances are given in Table 6. It may be noted that the variances are different between 6 materials, but are almost the same between testing methods. For the data, we examined three models  $M_1, M_2$  and  $M_3$ . The results on MLE's, AIC and CAIC are given in Table 7. The sample sizes  $n_{ij}$  are all 6, and are relatively small. So, we use CAIC. As a result, it is concluded that  $M_2$  is appropriate.

Table 6. Means and variances							
i	j	$n_0$	mean	variance			
1	1	6	0.07627	0.00007			
	2	6	0.20938	0.00131			
	3	6	0.21278	0.00428			
	4	6	0.71098	0.02323			
	5	6	1.92135	0.03125			
	6	6	1.10768	0.03085			
2	1	6	0.06138	0.00016			
	2	6	0.15183	0.00146			
	3	6	0.24127	0.00315			
	4	6	0.77772	0.00428			
	5	6	2.34835	0.11399			
	6	6	1.17220	0.13070			

Table C. Manua and main

#### Table 7. MLE, AIC and CAIC

	d	$\alpha$	$\gamma \text{ or } \beta$	AIC	CAIC
$M_1$	13		1.039820	-130.5692	-125.5097
$M_2$	14	-0.029578	1.161379	-140.6882	-134.4448
$M_3$	18			-140.9095	-130.9095

### 6 Conclusion

In this paper, we considered some linear structure models with different variances, based on the data (Kanai et al. (2007)) measured for different materials by two fracture toughness testing methods. More precisely, we considered three types of structures between two testing methods, which are denoted by  $M_1, M_2$  and  $M_3$ . For selection of these models, we gave AIC, and further, we derived its corrected version, CAIC. It was pointed that CAIC is more effective than AIC in the case of small samples, based on simulation experiments. Based on our results, it was pointed that there is a linear structure between two fracture toughness testing methods.

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